

# 200 $\Omega$ Chopper R&D Progress

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Project X collaboration meeting

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- Development approach and objectives
  - Subsystem development progress
    - Vendor contributions
    - Status of driver development
  - Summary

## 200 $\Omega$ approach pros and cons



- Pros
  - Lower power dissipation in the driver, kicker structure and load
  - We have chosen for the driver to be DC coupled to avoid base line shifting of AC coupling
- Cons
  - Neither a driver, nor 200  $\Omega$  transmission lines, feed-throughs, or load are commercially available

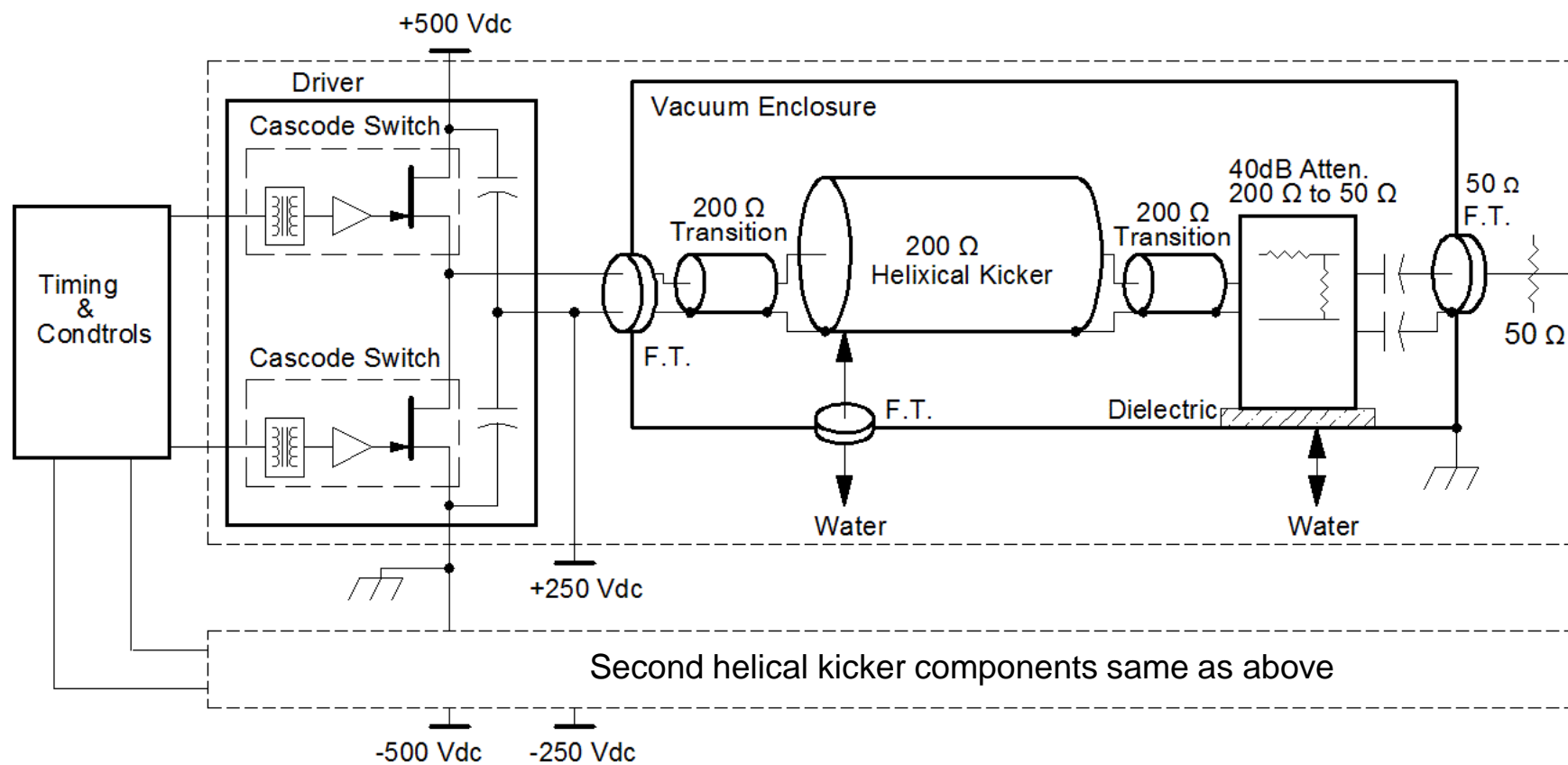


- Present design effort targets these objectives
  - Potential to reach 500 V
  - Switch either of two chopping schemes
    - Two 500 volt kickers to kick beam out
    - Or, two +/- 250 volt kicker to kick beam both in and out
  - DC coupled drive to the kicker
  - ~2 ns rise time
  - Be able to kick out one bunch (~1.5 ns wide flat top)
  - Handle power dissipation for high duty factor
  - Support variable high duty factor waveforms
  - Handle rep rates, ~30 MHz

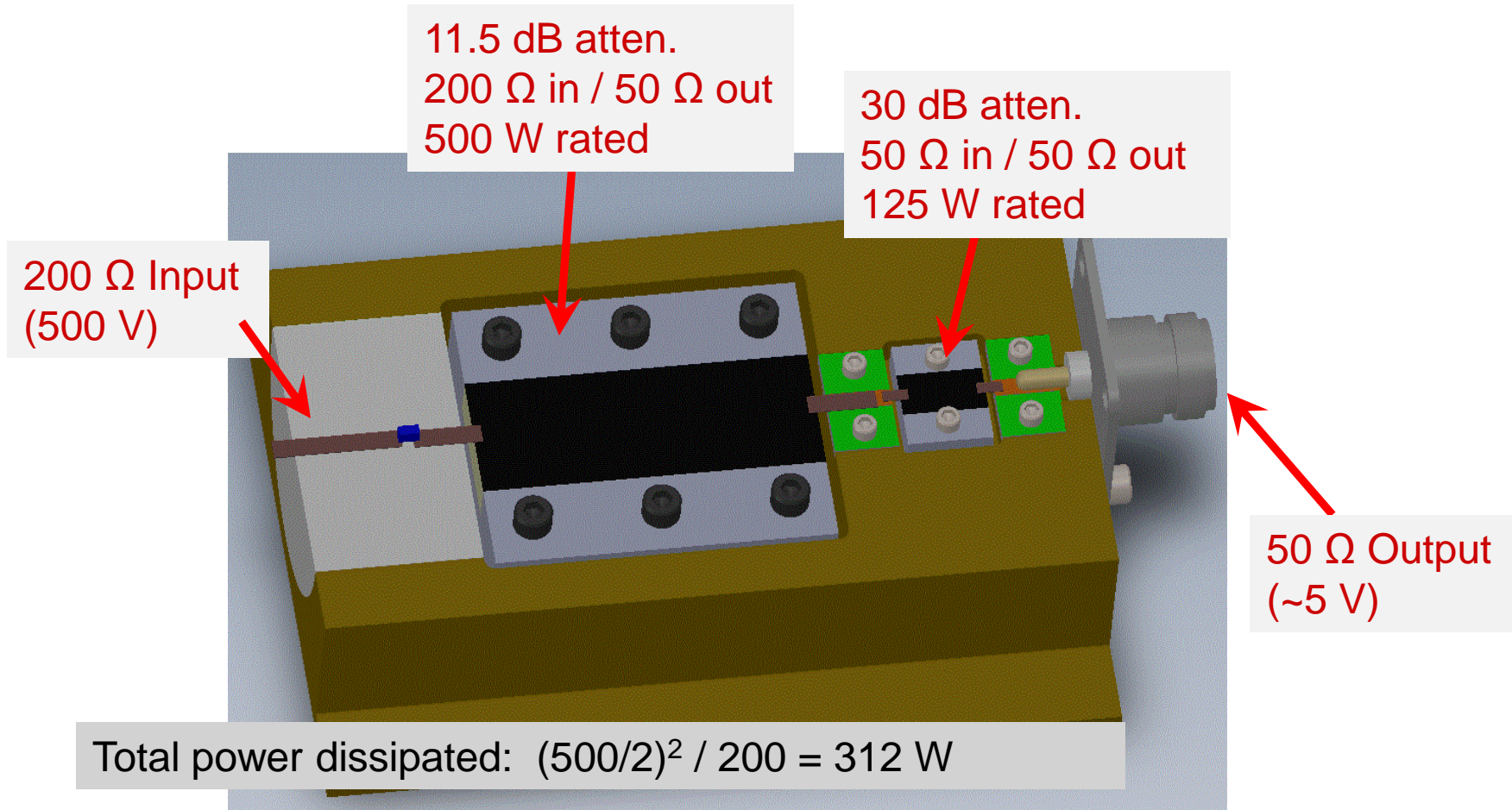
# System block diagram as currently proposed



Two helical kickers: their interconnections and biasing



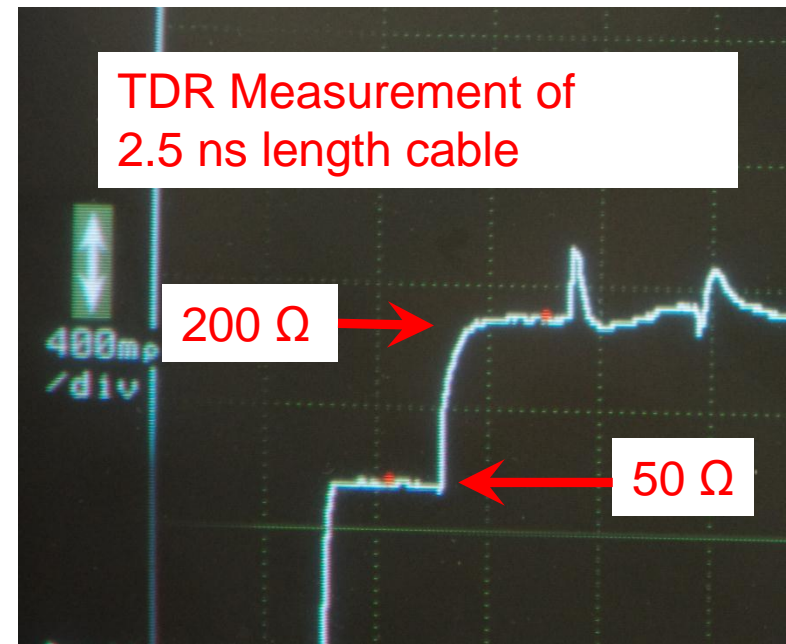
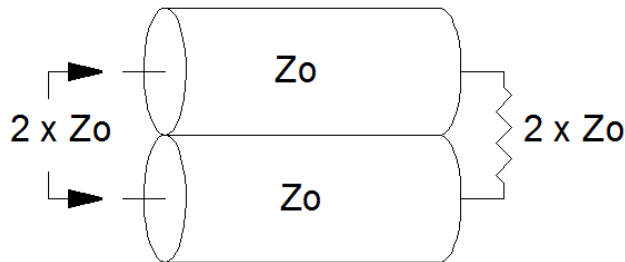
## 200 $\Omega$ termination prototype designed by Elab, Inc.



Total power dissipated:  $(500/2)^2 / 200 = 312 \text{ W}$



- Transmission line options
  - Home made coax
  - Home made microstrip line
  - Dual 100  $\Omega$  coax
- Dual 100  $\Omega$  coax under evaluation

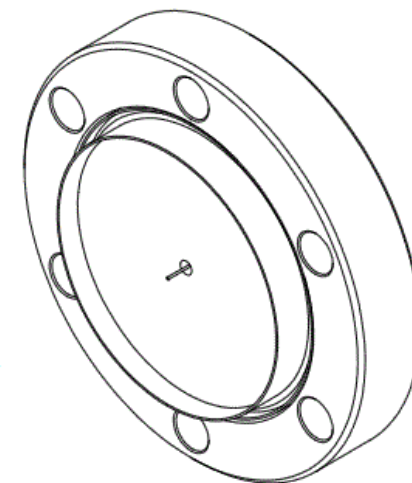
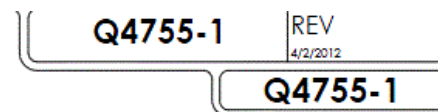
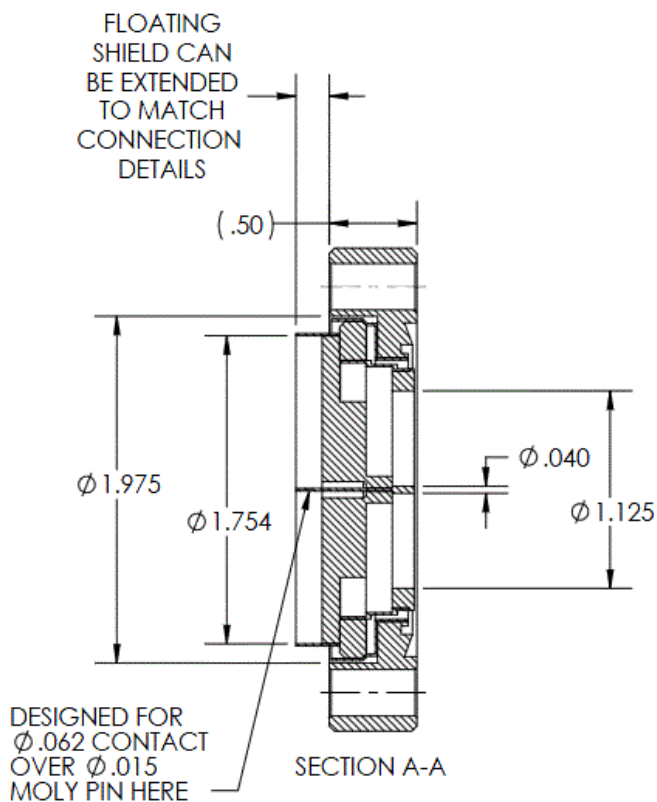
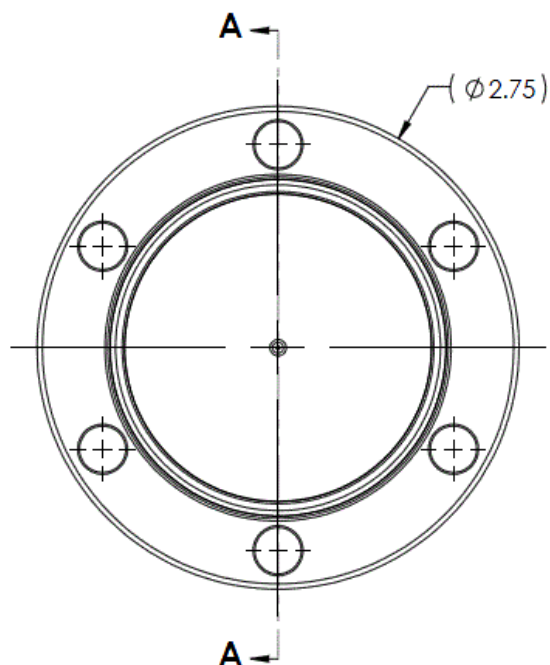


- Measurement shows 0 – 1.75 ns rises from 125  $\Omega$  to ~200  $\Omega$
- Use may require additional compensation
- 100  $\Omega$  coax supplied by Haverhill Cable

# Custom feedthru by MPF Products, Inc.



Low capacitance isolated  
feedthru

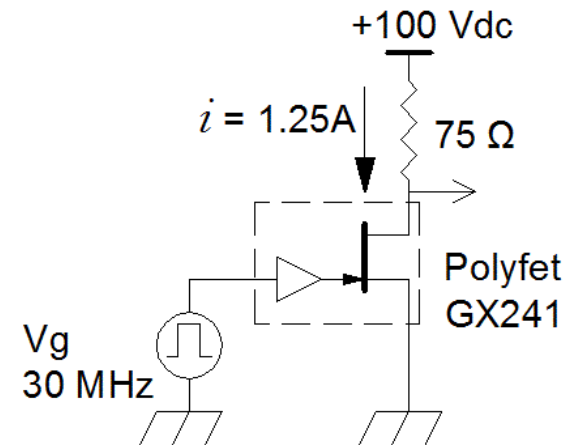




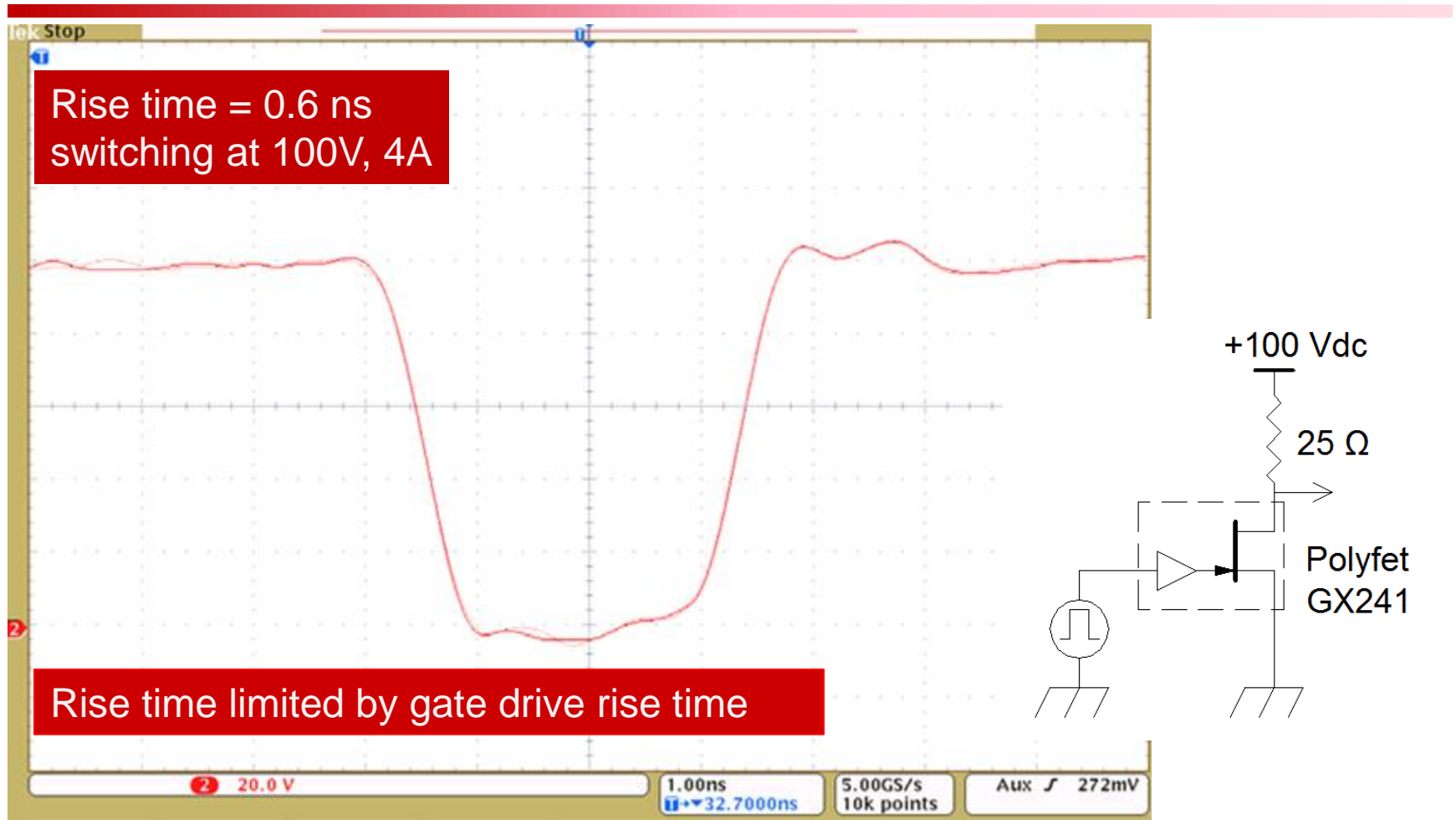
# Driver: GaN FET switching power



- GaN FET power dissipation test
  - Switched at 30 MHz CW
  - Duty factor = 50 % (62 W delivered)
    - Case temp = 86 °C
  - Duty factor = 25% (31 W delivered)
    - Case temp = 81 °C
- Test performed without a heat sink
  - FET soldered to G-10 PCB
  - No forced air flow over the transistor
- Conclusions
  - Switching losses dominate over conduction losses at 30 MHz
  - Obtaining adequate cooling should be possible

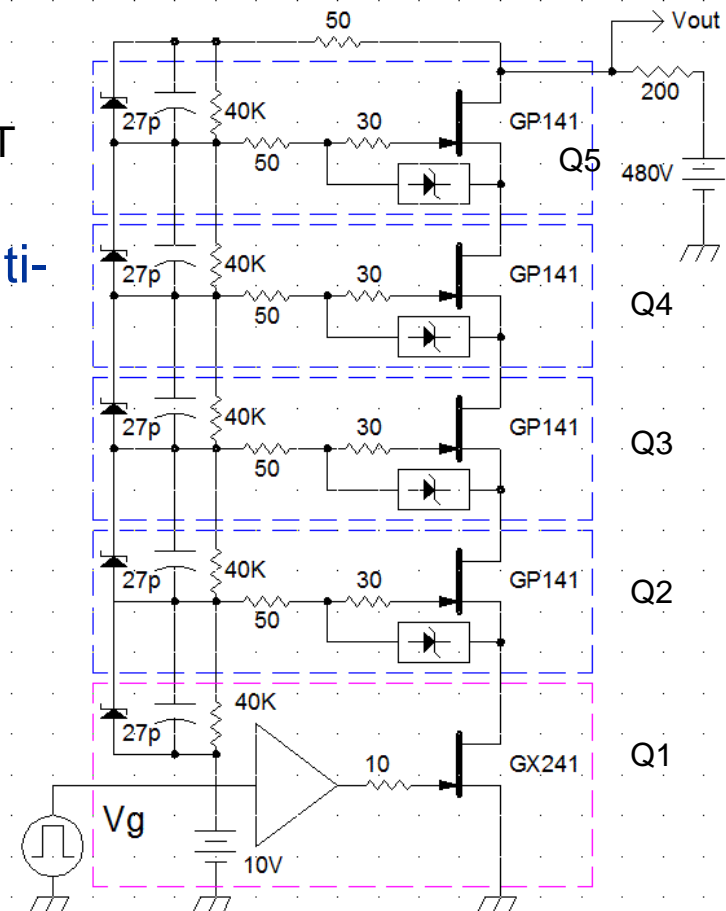


Gx241 specs:  
 $C_{oss} = 8.5 \text{ pF}$   
 $B_{vds} = >200V$

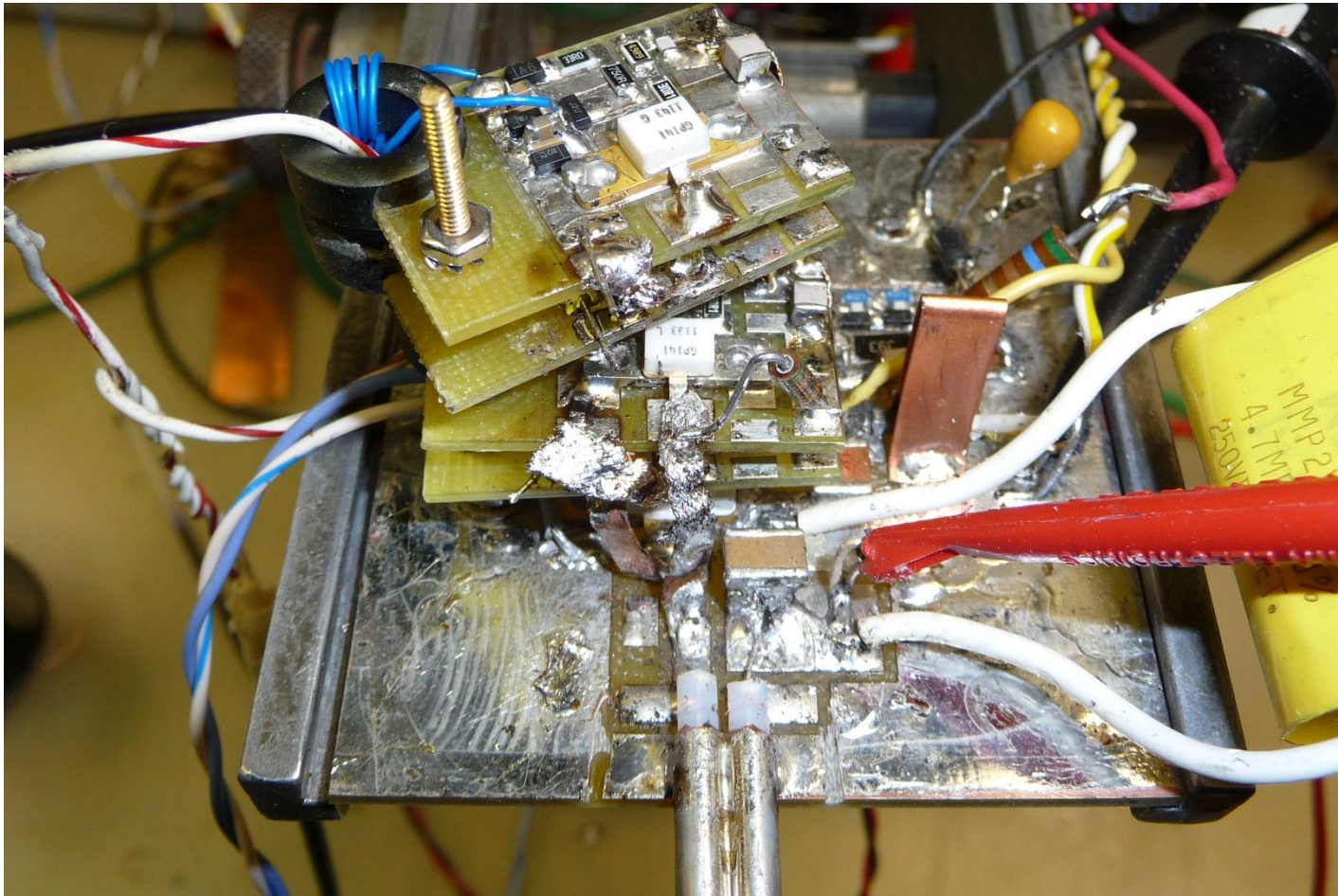




- Motivation for multi-FET circuit
  - Currently available devices limited to 200 V
  - However, switching losses at 100 V per FET are more manageable
- The appeal of cascode scheme for multi-FET switch
  - FETs turn on together and share voltage
  - There is only one control signal
  - Has the potential of switching fast
- Major components
  - 1 common source driver stage (Q1)
  - 4 common gate stages in cascode (Q2-Q5)
  - RC divider string forces voltage sharing
  - Voltage clamps protect Q2-Q5 gates



## 5 FET Cascode switch

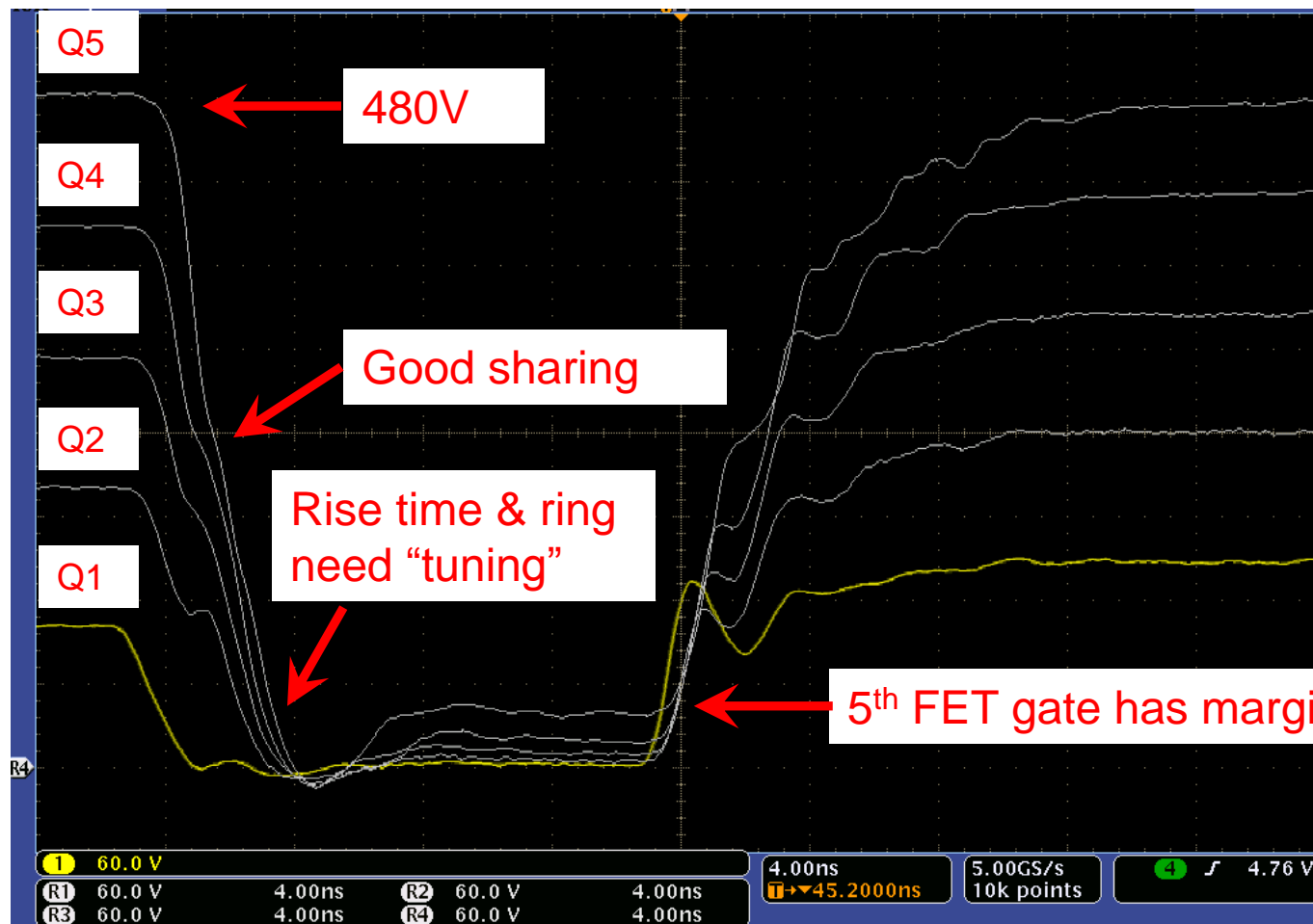




- Major issues
  - Design common source driver stage having  $<1$  ns rise/fall time
  - Provide adequate gate drive voltage in the common gate stages
    - During edges while turn on
    - Gate drive level decreases on upper FETs
  - Minimize output overshoot and ring
- Minimize and counteract parasitic capacitance and inductance
  - Increase FET switching losses
  - Responsible for output overshoot and ring
  - Impair output rise time

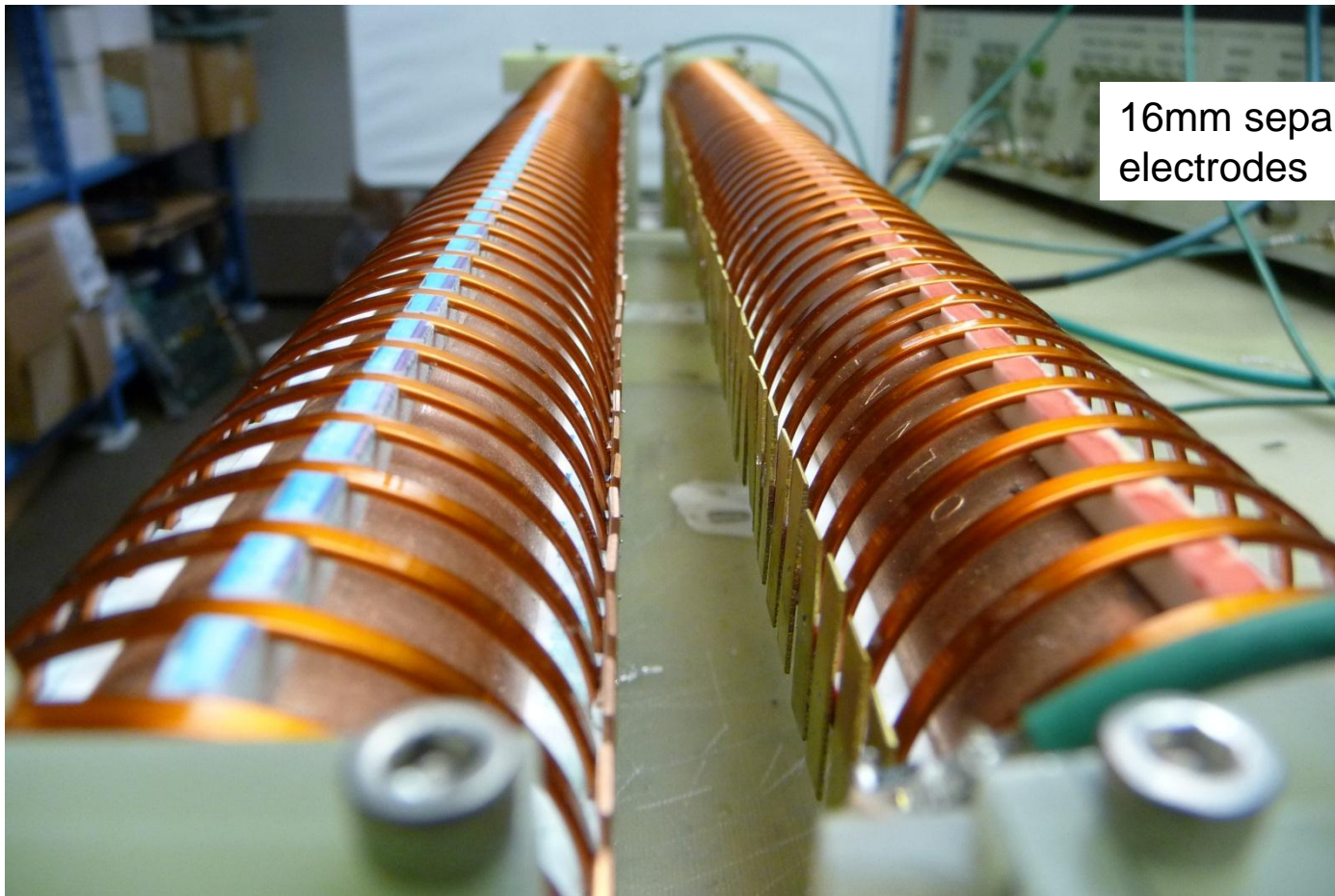


# Switching to 480 V

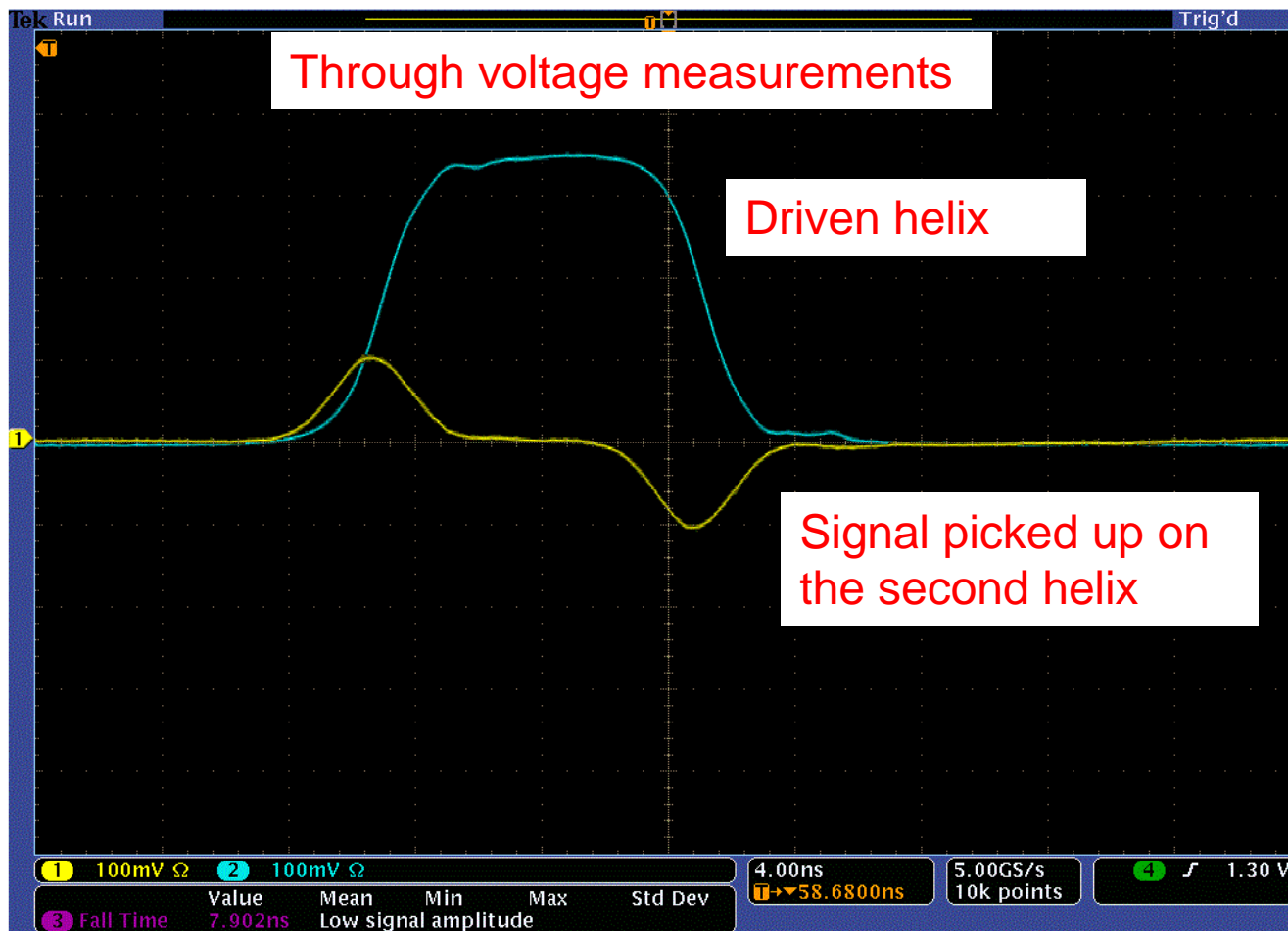


Ferrite beads in drain circuits dampen overshoot and ring

## Two helixes 16mm appart



# Coupling effect

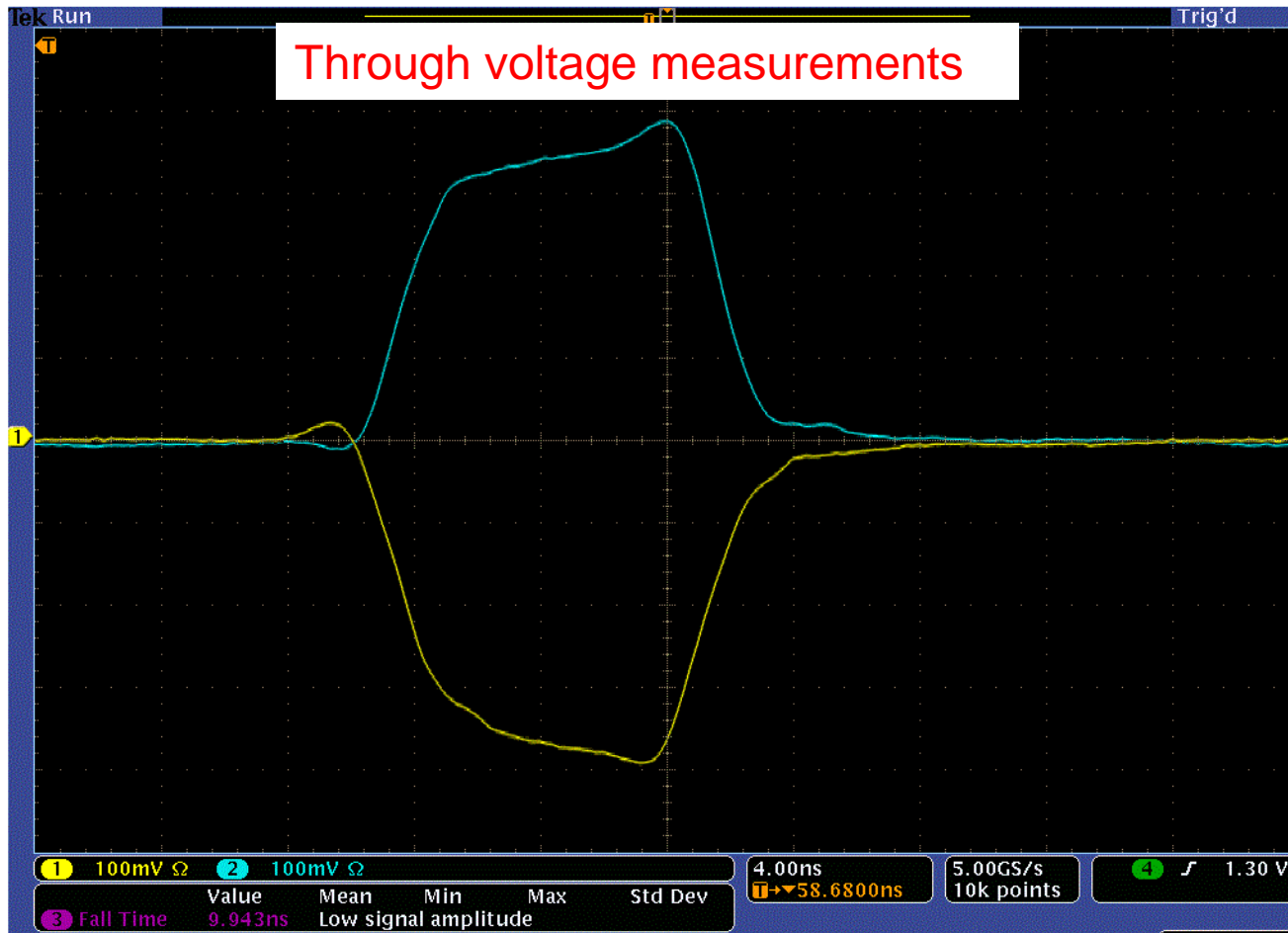


Driver = 2 ns  
rise/fall

Both helixes are  
resistively  
matched to 50  $\Omega$

Both helixes  
wound in the  
same direction





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- All subsystems have are under development to some degree
    - Mechanical Support Dept. is working on kicker design
    - 200  $\Omega$  transmission lines are under evaluation
    - One feed thru vendor has submitted one proposal
    - We are to receive 200  $\Omega$  termination prototype in April
  - Driver design is approaching 500 V